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Supporting Information for

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**Frictional and Hydraulic Properties of Plate Interfaces Constrained by**

5

**a Tidal Response Model Considering Dilatancy/Compaction**

6

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## 16 **Introduction**

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 24 drained model.  
 25 Figure S4 shows the numerical solution of  $c$  in equation (12) for the drained model.

26

27 **Text S1. Derivation of governing equations for the drained model**

28 We explain a drained model in which pore fluids flow out of the shear zone (Figure S1b). The  
 29 difference between the undrained and drained models is in the presence of fluid flow. The  
 30 governing equations of the drained model are the same those as in the undrained model  
 31 (equations (3), (4) and (8)), except for the governing equation for pore fluids.

32 Following the work of Segall et al. (2010), we assume homogeneous diffusion (HD), which  
 33 holds under the condition that  $T \gg t_w$ . In the HD case, the effect of the finite shear zone  
 34 thickness can be neglected, so the width of the shear zone can be formally defined as  $w \rightarrow 0$   
 35 (Segall et al., 2010). The direction of fluid flow (Figure S1b) is parallel to the  $z$ -axis, and the  
 36 shear zone lies on  $z = 0$ .  $c_{hyd}$  denotes the fluid pressure diffusivity at  $z \neq 0$ . Then, the  
 37 governing equation for pore fluids can be written as (Segall et al., 2010)

$$\frac{\partial p}{\partial t} = c_{hyd} \frac{\partial^2 p}{\partial z^2} \left( \frac{\partial p}{\partial z} \Big|_{z=0} = \frac{Mw\dot{\phi}}{2c_{hyd}} \right) \#(S1)$$

38

39 **Text S2. Nondimensionalization of the governing equations in the drained model**

40 The governing equations for the drained model are the upper three in equation (10) and the  
41 nondimensionalized equation (S1). When we adopt  $\sqrt{c_{hyd}T}$  as the representative length in the z-  
42 axis direction, the nondimensionalized equation (S1) can be written as

$$\frac{\partial \tilde{p}}{\partial \tilde{t}} = \frac{\partial^2 \tilde{p}}{\partial \tilde{z}^2} \left( \frac{\partial \tilde{p}}{\partial \tilde{z}} \Big|_{\tilde{z}=0} = -E_p \frac{1}{\tilde{\theta}} \frac{d\tilde{\theta}}{d\tilde{t}} \right), \#(S2)$$

43 where  $E_p = M\epsilon/2\sigma_{eff}^0 \sqrt{w^2/Tc_{hyd}} = U/2 \sqrt{w^2/Tc_{hyd}}$ .  $E_p$  represents the relative importance of  
44 the dilatancy/compaction effect to the effective normal stress change in the drained model.  
45 Previous experiments and observations suggest that  $c_{hyd} \sim 10^{-1\sim 3}$  m<sup>2</sup>/s (Yamashita and  
46 Tsutsumi, 2018) and  $U \sim 10^{0\sim -2}$  (Section 2.2.3). Using  $10^{0\sim 1/2}$  m as the value of  $w$  (Section  
47 4.3.4), we obtain a possible range of  $E_p$  of  $10^{-2}$  to  $10^{-4}$ .

48

49 **Text S3. A numerical method for the governing equation in the drained model**

50 The upper three equations in equation (10) are calculated numerically using the third-order  
51 Adams-Bashforth method. equation (S2) is calculated numerically using the method in Appendix  
52 B of Segall et al. (2010). In the following, we discuss the latter method. Near the shear zone, the  
53 discretization needs to be sufficiently fine to capture a steep gradient of the pore fluid pressure.  
54 On the other hand, for a region far from the shear zone, the discretization does not need to be fine  
55 because the pore fluid pressure gradient is small. Thus, we use the following coordinate  
56 transformation between  $z$  and  $r$  (Segall et al., 2010):

$$z(r) = -c + e^r \text{ or, equivalently } r(z) = \ln(c + z).$$

57 We solve equation (S2) numerically in a new coordinate system using the Crank-Nicolson  
58 method. Specifically, we solve

$$\left\{1 + \frac{\gamma}{2} e^{-r_k} (e^{-(r_k-\delta)} + e^{-(r_k+\delta)})\right\} p_k^{i+1}$$

$$= p_k^i + \frac{\gamma}{2} e^{-r_k} e^{-(r_k-\delta)} (p_{k-1}^i + p_{k-1}^{i+1}) - \frac{\gamma}{2} e^{-r_k} p_k^i (e^{-(r_k-\delta)} + e^{-(r_k+\delta)}), \#(S3)$$

59 where  $\gamma = \Delta t / \Delta r^2$ ,  $\delta = \Delta r / 2$ , and  $p_k^i$  is the value of the pore fluid pressure of the  $k$ -th grid in  
60 the new coordinate system at time step  $i$ .  $\Delta t$  and  $\Delta r$  represent increments in time and space,  
61 respectively. In this study, the number of grids is 35, the starting position of the grid is  $r(0) =$   
62  $\ln(0)$ ,  $\Delta r = 0.3$ , and  $c = 10^{-4}$ . Therefore, the grid farthest from the shear zone in the numerical  
63 calculation using  $c_{hyd} \sim 10^{-1} \text{ m}^2/\text{s}$ ,  $T \sim 12.4 \text{ h}$  is approximately  $z=170 \text{ m}$ , while the grid farthest  
64 to the shear zone in the numerical calculation using  $c_{hyd} \sim 10^{-3} \text{ m}^2/\text{s}$ ,  $T \sim 12.4 \text{ h}$  is  
65 approximately  $z=17 \text{ m}$ .

66

#### 67 **Text S4. The approximate solution of the tidal response for the drained model**

68 The approximate solution for the drained model is derived in the same manner as in Section 3.1.  
69 The pore fluid pressure change due to fluid flow is represented as  $p(z, t) = p_0 + \Delta p(z) e^{i\omega t}$ ,  
70 where  $p(0, t)$  corresponds to the pore fluid pressure in the shear zone. The equations for the  
71 drained model corresponding to equations (13) and (14) for the undrained model are

$$\frac{\Delta \tilde{V}}{\tilde{V}_{pl}} = \frac{2\pi i}{\tilde{K} \tilde{V}_{pl} + 2\pi i C} |\Delta \tilde{S}(t)| \#(S4)$$

72 and

$$C = a - \frac{1}{1 + i \frac{T_\theta}{T}} (b - \mu_{pl} E_p \sqrt{2\pi i}), \text{ respectively. } \#(S5)$$

73 The equations of the drained model corresponding to equations (17) and (18) for the undrained  
74 model are

$$\alpha = Re \left( \frac{2\pi i}{(\tilde{K} \tilde{V}_{pl} + 2\pi i C) \sigma_{eff}^0} \right) \#(S6)$$

75 and

$$\delta = \arg\left(\frac{2\pi i}{\tilde{K}\tilde{V}_{pl} + 2\pi iC}\right), \text{ respectively. \#(S7)}$$

76 Furthermore, by applying the argument from which equations (19) and (20) were derived for the

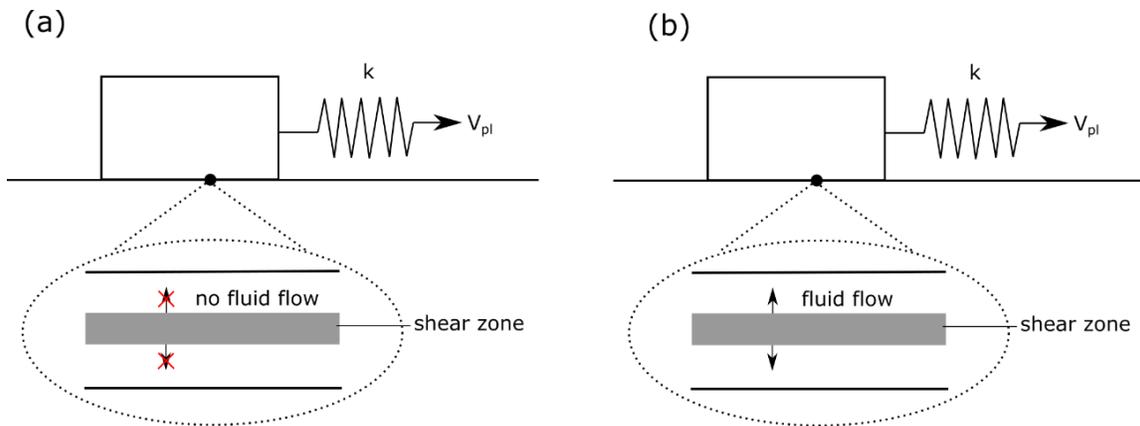
77 drained model, the approximate solutions of  $\alpha$  and  $\delta$  can be expressed as

$$\alpha \sim \text{Re}\left\{(C\sigma_{eff}^0)^{-1}\right\} \#(S8)$$

78 and

$$\delta \sim \arg\{C^{-1}\}, \text{ respectively. \#(S9)}$$

79

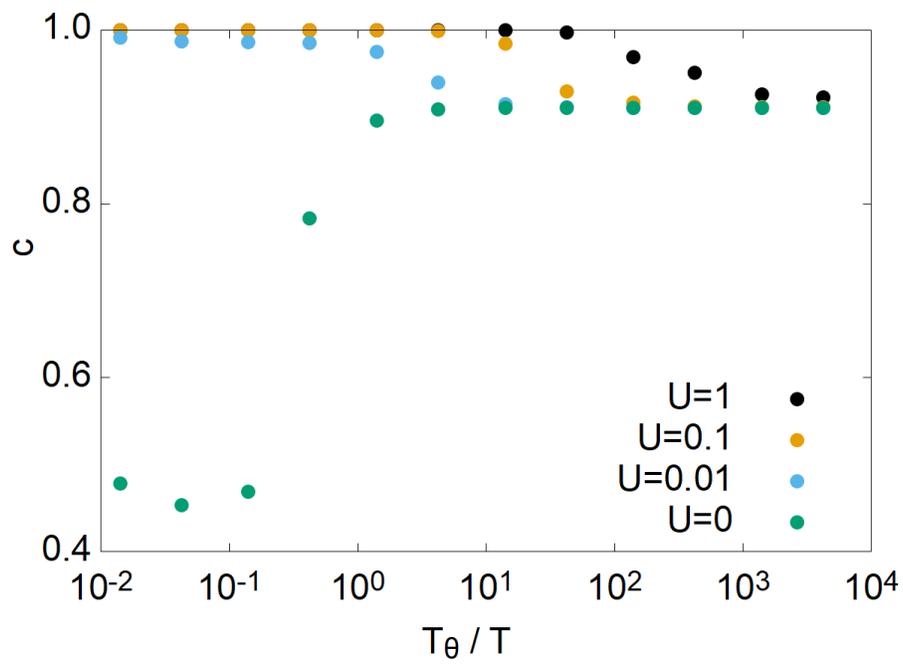


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81 Figure S1. A schematic of the undrained (a) and drained (b) models. The difference between the  
 82 two models is whether fluid flows outside the shear zone.

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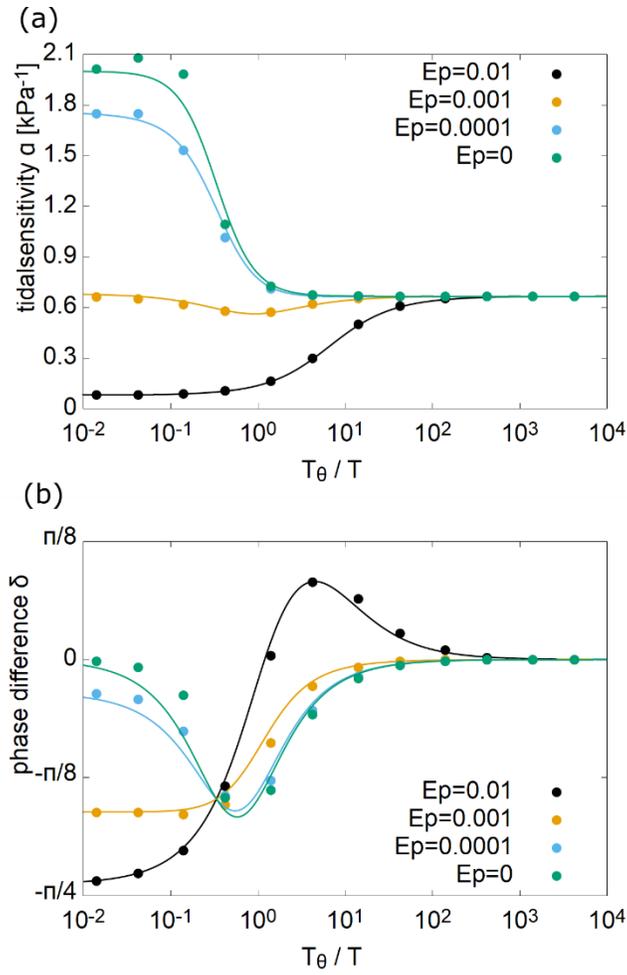


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86 Figure S2. The numerical solution of  $c$  (dots). The differences in color represent differences in the  
 87 dilatancy parameter  $U$ .

88

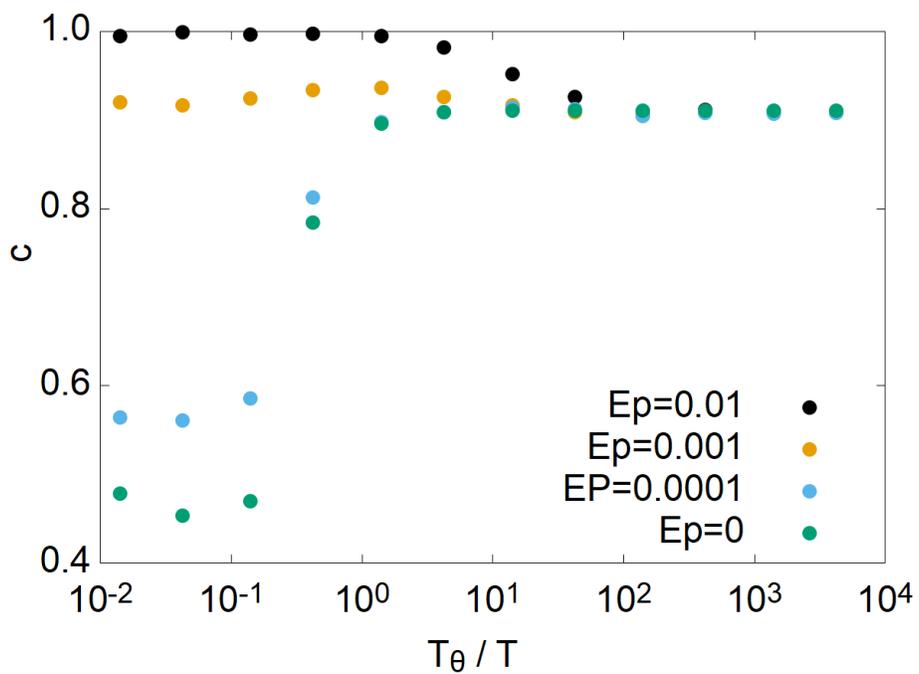
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90

91 Figure S3. (a) The numerical solution of  $\alpha$  (dots) and the approximation solution (i.e., equation  
 92 (S8)) (solid line). (b) The numerical solution of  $\delta$  (dots) and the approximation solution (i.e.,  
 93 equation (S9)) (solid line). The differences in color represent differences in the dilatancy  
 94 parameter  $E_p$  for the drained model.

95



96

97 Figure S4. The numerical solution of  $c$  (dots). The differences in color represent differences in the  
 98 dilatancy parameter  $E_p$  for the drained model.

99